

Number 10

Removal of 4-Chlorophenoles from Simulated Wastewater by Advanced Oxidation Processes

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Abstract

The degradation and mineralization of 4-chlorophenol (4-CP) by advanced oxidation processes (AOPs) was investigated in this work, using both of UV/H₂O₂ and photo-Fenton UV/H₂O₂/Fe⁺³ systems. The reaction was influenced by the input concentration of H₂O₂, the amount of the iron catalyst, the type of iron salt, the pH and the concentration of 4-CP.

A colored solution of benzoquinon can be observed through the first 5 minutes of irradiation time for UV/H₂O₂ system when low concentration (0.01mol/L) of H₂O₂ was used. The colored solution of benzoquinon could also be observed through the first 5 minutes for the UV/H₂O₂/Fe⁺³ system at high concentration (100ppm) of 4-CP. The results have shown that adding Fe⁺³ to the UV/H₂O₂ system enhanced the rate of 4-CP oxidation at a molar ratio of H₂O₂/Fe⁺³/4-CP equals to 13/0.4/1 by a factor of 7. This reduced the consumption of H₂O₂ by a factor of 6 and the irradiation time required for complete degradation was reduced by a factor of 6. The experimental results have shown that the optimum reagents for a complete degradation of 4-CP(50ppm) were H₂O₂=0.005mol/L, Fe⁺³=0.16*10⁻³ mol/L under acidic condition (pH=3) and irradiation time of 15 min for the UV/H₂O₂/Fe⁺³/4-CP equals to 13/0.4/1.

Keywords: 4-chlorophenol; advance oxidation process; Fenton process; photo-Fenton process; UV photolysis.

الخلاصة

تم التحقق من فاعلية استخدام طرق الأكسدة الحديثة (AOPs) للنظامين $UV/H_2O_2/Fe^{+3}$ و $UV/H_2O_2/Fe^{+3}$ الكلور وفينول (H2-2) . التفاعل تأثر باختلاف الكميات المضافة من بيرو كسيد الهيدروجين (H2O_2)، كمية الحديد كعامل مساعد ، فو عية العامل المساعد Fe^{+3} و Fe^{+3} ، Ff و Fe^{+3} ، أو عبد المواد الملونة متمثلة بال (benzoquinone) تم ملاحظتها بعد 5دقائق من بدأ التجربة لنظام $UV/H_2O_2/Fe^{+3}$ ليبيروكسيد الهيدروجين (MO-L)، كذلك تم ملاحظتها بعد 5دقائق من بدأ التجربة لنظام $UV/H_2O_2/Fe^{+3}$ ملاحظتها بعد 5دقائق من بدأ التجربة لنظام $UV/H_2O_2/Fe^{+3}$ عند استعمال تركيز قليل لبيروكسيد الهيدروجين (Mole 10.01 mole). كذلك تم ملاحظة ظهور المواد الملونة بعد 5 دقائق من بدأ التجربة لنظام $UV/H_2O_2/Fe^{+3}$ عند استعمال تركيز قليل لبيروكسيد الهيدروجين (Mole 10.01 mol/L). كذلك تم ملاحظة ظهور المواد الملونة بعد 5 دقائق من بدأ التجربة لنظام $V/H_2O_2/Fe^{+3}$ عند استعمال تراكيز عالية من الكلوروفينول (pm100). النتائج بينت ان إضافة الحديد (Fe⁺³) كعامل مساعد الى لنظام $V/H_2O_2/Fe^{+3}/4-CP$ وبنسبة مولارية 10.0/1 ل (pm100). النتائج بينت ان إضافة الحديد (Fe⁺³) كعامل مساعد الى لنظام $H_2O_2/Fe^{+3}/4-CP$ وبنسبة مولارية 10.0/1 ل لازمن اللازم اللازم وليونول الكلوروفينول الموسول الى التحال العلى بمقدار 7 مرات وأدت إلى تقليل مادة إلى $PO^{-2}/Fe^{+3}/4-CP$ ppm (50.01 mol/L). النتائج بينت ان إضافة الحديد (H2O_2=0.005mol/L (Fe⁺³) وبنسبة مولارية 11.0/1 ل لازمن اللازم هي 11.0/1 ل وسول الى التحال الكامل انخفض بمقدار 6 مرات التراكيز المثلى اللازمة للحصول على تحلل كامل للكلوروفينول بتركيز 50.0 mol/L (H2O_2) وبنسبة مولارية 11.0/1 ل ولا مال الحمول الى التحال الحلي المولي الموسول الى التحال الكامل الكلوروفينول بتركيز 70.000 mol/L (Fe⁺³)</sup> وبنسبة مولارية 11.0/1 (10.000) ولا الحمول الى التحال الكامل الكلوروفينول بتركيز 70.000 mol/L (Fe⁺³)</sup> وبنسبة مولارية 11.0/1 (10.000) ولا الحمول الى التحال الحمول على تحلل كامل الكلوروفينول بركيز 70.000 mol/L (Fe⁺³)</sup> وبنسبة مولارية 11.000) وبنسبة مولارية 11.000 (10.0000) وبنسبة مولارية 11.000 (10.00000) ولا الحمول الحمول ولى ا

1. Introduction

The need to restore contaminated sites to avoid further damage to the environment has raised the development of effective methods for pollutants removal in the last years. The treatment processes for different types of effluents must guarantee the elimination or recuperation of the pollutants in order to reach the strict authorized levels for their discharge, (Weber and Smith, 1986).

An ideal waste treatment process must completely mineralize the toxic species present in the waste streams without leaving behind any hazardous residues and should be cost-effective as well, (Stoyanova et al., 2003).

Chlorophenols are highly toxic and cause considerable damage to the ecosystem and human health. They are notified as potential toxic compounds by United State Environmental Protection Agency (USEPA) and their maximum allowable concentrations in drinking-water as total chlorophenols are 0.1ppb (WHO, 2008).

They are introduced into the environment as a result of several man-made activities, e.g. water disinfection, waste incineration, uncontrolled used of pesticides and herbicides, as well as by-products in bleaching of paper pulp with chlorine (Pera-Titus et al., 2004).

Chlorophenols are designated as the priority pollutants by the USEPA and European Commission (Kralik et al., 2009).All chlorophenols possess bactericidal activities that increase with the degree of chlorination. Chlorophenols are highly toxic to algae. Most plants are very sensitive to the phytotoxicity of chlorophenols. As for aquatic organisms, fish and other aquatic organisms absorb chlorophenols through their gills, gastrointestinal tract or skin (WHO, 1998).

The conventional pollutant destructive technologies include biological, thermal and physiochemical treatments. On most occasions, biological treatments require long residence time for microorganisms to degrade the pollutant because they are affected by the pollutant toxicity. Thermal treatments present considerable emission of other hazardous compounds. Other techniques such as flocculation, precipitation, adsorption, air stripping or reverse osmosis (RO) require posttreatment to remove the pollutant from the newly

Removal of 4-Chlorophenoles from Simulated Wastewater by Advanced Oxidation Processes

contaminated environment. Alternative methods to these well-established techniques are the so-called advanced oxidation processes. AOPs are based on the initial formation of radicals, i.e., hydroxyl radicals (OH \cdot) that later act as non-selective oxidation agents.

The possible reaction pathways involving the attack of hydroxyl radicals onto organic compounds are: the electrophylic addition of a hydroxyl radical to organic compounds (unsaturated or aromatic) leading to the formation of organic radicals (Equation 1), the hydrogen abstraction by reacting the hydroxyl radical with a saturated aliphatic compound (Equation 2) and electron transfer with reduction of the hydroxyl radical into a hydroxyl anion by an organic substrate (Equation 3), (Tang , 2004).

$HO' + \longrightarrow or \bigcirc \rightarrow HO \longrightarrow or \bigcirc OH$	(1)
$HO' + R - H \rightarrow R' + H_2O$	(2)

$\text{HO}^{+} + \text{R} - \text{X} \rightarrow [\text{R} - \text{X}]^{+} + \text{HO}^{-}$	(3)
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Several technologies are included in the AOPs like Fenton, photo-Fenton, wet oxidation, ozonation, photo catalysis...etc. and the main difference between them is the manner to form the radicals. Even though these techniques can provide the conversion of contaminants to less harmful compounds, on most occasions, oxygenated organic products and low molecular weight acids are formed throughout the process. In addition, advanced oxidation processes are limited to treat waters which contain low concentrations of organic or inorganic scavenging substances. Experiences with different oxidation technologies and substrates have shown that partial oxidation of toxic water may increase its biodegradability up to high levels (Pera-Titus et al., 2004).

Advanced oxidation technologies (AOPs) have received increased interest (Kralik et al., 2009). Alnaizy et al., (2000) studied phenol degradation with a UV/H₂O₂ process in a completely mixed, batch photolytic reactor, the UV irradiation source was a low-pressure mercury lamp. The study indicates that there is an optimum H₂O₂ /phenol molar ratio for efficient degradation in the range of 100-250.



Hirvonen et al., (2000) made a comparison between 2, 4-dichlorophenol degradation rate by UV/H_2O_2 process and direct UV (20-W 254 nm lamp) irradiation, in the study they reported that the addition of hydrogen peroxide at acidic pH increased the reaction rate by one order of magnitude.

Munter (2001) used AOP to oxidize inorganic contaminants such as cyanide, sulphide and nitrite.

Carneiro et al., (2006) show that typical Fenton catalyst/ H_2O_2 ratios range is 1:5 to 1:25; they proven that the optimal pH range for Fenton process is between 2.8 and 3.0.

Matilainen and Sillanp (2010) noted that the degradation of target compounds with UV/ H_2O_2 and VUV (λ =172nm) occur about eight times more effectively than with direct UV-photolysis.

Kuo and Wu, (2010) investigate the effect of solar irradiation on Fenton degradation of 4-chlorophenol. The results indicated that solar assisted photo-Fenton process was effective for complete removal of 4-chlorophenol in water. More than 90% of 4-chlorophenol was mineralized to CO_2 in solar assisted process while only 25% carbon mineralization was observed in Fenton process.

Bogatu et al., (2005); Nogueira et al., (2008); Murcia et al. 2009; and Elghniji et al., (2011) identified the intermediate generated during the photocatalytic process of phenolic compounds. The major intermediates are benzoquinone and hydroquinone .The concentrations reach а maximum and then tend to decrease gradually for longer irradiation time indicating the mineralization of these compounds.

The objective of this work is to study the effectiveness of the AOPs in the degradation of 4-chlorophenol as one of the main compounds of the chlorophenols, using pilot plant scale. The AOPs selected to carry out this study were, UV/H_2O_2 and photo-Fenton ($UV/H_2O_2/Fe^{+3}$) systems. To achieve the experimental objectives, different variables were chosen to be followed throughout the treatment: 4-chlorophenol concentration, pH, H_2O_2 and Fe⁺³ concentrations.

2. Materials and Methods

2.1. Reagents

4-Chlorophenol (4-CP) was used as a model substance employed in this research. The physical, chemical, UV-visible absorption spectra and molecular structure of 4-CP are shown in Table 1 and Fig.1, (Thomas and Burgess, 2007). Table 2 shows all the chemicals that were used in the experimentation. All were analytical grade and used as received. All the solutions were prepared by dissolving requisite quantity in distilled water. The pH of the solution was adjusted using H_2SO_4 solution. Initial pH of solution was monitored using a pH meter from (WTW Co., Germany, INOLAB 720).

2.2. Equipments

A laboratory scale set up of AOPs system applied in this study is presented in Fig. 2.(Shihab, ,2011). The reactor (1) was made entirely of aluminum with an effective volume of 37.5L. A feed tank (5) of 24L volume was used to prepare the solutions .The solution was circulated at flow rate of 3L/min by using a water pump (3) of 0.5Hp and 0.37kw (Marquis Co., China) .To measure the flow rate, a calibrated flow meter (4) of Hidrotek type with flow range (3 to 20L/min) was used. This flow meter was installed vertically and the flow direction was upward. Valves were utilized for sampling, washing, drain and control in the AOPs system as illustrated in Fig.2. A photograph of the photo reactor is shown in Fig. 3. The inlet and outlet pipes were 1.8cm diameter. Vertical baffles were fixed after the inlet zone to let the water overflow to increase the mixing. Two vertical plates with ten rectangular openings (13x1cm) were used as distributors. Three removable side baffles were fixed vertically at the reactor side walls. These baffles are with square cross sectional area with a side length of 5 cm. These baffles reduce the presence of low radiation zones near the reactor walls. UV radiation was generated from three UV lamps TUV 11W 4P-SE (4-Pin single ended), these lamps emit output power at a wavelength of 253.7nm and each was sheathed in a quartz sleeve for protection. These lamps were fixed in a staggered form in the reactor. The spacing between two adjacent lamps should be in a range between (5-12) cm. If this distance is less than 5cm then the

Yasmen A. Mustafa Ahmed H. Shihab

UV energy will be absorbed by the adjacent UV lamp, if the spacing is more than 12cm, there will be a formation of a zone with low UV intensity between the lamps (Chiu et al., 1999; Lyn and Blatchley, 2005). In this study 10cm spacing was used.





Fig.1:UV-visible spectra for the 4-CP at different pH values(Thomas and Burgess, 2007).



Fig.2:A laboratory scale set up of AOPs system.(1)AOPs reactor,(2)sample extraction valve (3) water pump (4)flow meter (5)feed tank (waste water) (6)washing water inlet valve,(7)drain valve, and (8,9 and 10)control valves.

Removal of 4-Chlorophenoles from Simulated Wastewater by Advanced Oxidation Processes



Fig.3: A photograph of the AOPs reactor.

Table 2 : List of chemicals us

Compound	Formula	Vendor	
Hydrogen peroxide	H_2O_2	Scharlau (50 % wt/wt)	
Ferrous sulphate heptahydrate	FeS0 ₄ .7H ₂ 0	Thomas Baker (98 % purity)	
Ferric sulphate heptahydrate	Fe ₂ (SO ₄) ₃ .7H ₂ O	Thomas Baker (99.5 % purity)	
Sulfuric acid	H ₂ SO ₄	BDH (97 % purity)	
Sodium thiosulfate pentahydrate	$Na_2 S_2 O_3.5H2O$	Riedel Seelze Hannover (99 % purity)	

2.3. Experimental Procedure

The experimental procedure used in this research was as follows:

-The desired concentration of 4-CP was prepared and the pH was adjusted by adding a dilute H_2SO_4 solution in the feed tank.

- well mixing was maintained by using a mechanical stirrer for 5min.

-Initial sample (sample at time zero) was taken for analysis.



-The pump was switched on and the solution was allowed to flow from the feed tank through the pump to the photoreactor. Valves No. 2, 7 and 6 were closed and all the other valves were opened.

-The head in the photoreactor was maintained at 15cm by controlling the flow through valve No. 8.

-The desired quantity of H_2O_2 (0.01-0.05) mol/L was added to the feed tank. Circulation was allowed for few minutes then valve No.9 was closed.

-The UV light source was switched on.

-Samples were taken every 15 minutes through valve No.2 until the end of run. Samples were stored in 10 ml vials before analysis. One drop of $Na_2S_2O_3.5H_2O(0.1N)$ was added to each sample to decompose any residual hydrogen peroxide and prevent hydrogen peroxide from reacting with 4-CP during the analysis.

-For UV/H₂O₂/Fe⁺³ system, the same procedure was followed and the desired quantity of ferric sulphate was added in the feed tank before adding H₂O₂.

-The system was cleaned after the end of each run as follows:

The UV light source was turn off, the valves No.7 and 9 were opened leaving valves No.2,10 and 6 closed to drain the reactor and feeding tank. The system was washing by a tap water through valve No.6, by maintaining valve No.10 and 2 closed and valve No.7 opened for drainage.

UV-visible spectrophotometer (Model SP-3000 plus, Optima Co., 2003, Japan) was used to analyze the samples.

3. Results and Discussion

3.1. UV/H₂O₂ System

The combination of UV radiation and a little amount of H_2O_2 enhanced strongly the efficiency of degradation of 4-CP. Experiments were carried out at different doses of H_2O_2 (0.01-0.05) mol/L to study its effect on the degradation and mineralization of 4-CP. Fixed 4-CP concentration at 0.39*10⁻³mol/L (50ppm) was maintained during the experiments.

3.1.1. Effect of initial H₂O₂ concentration on UV/H₂O₂ system

Different concentrations of H_2O_2 (0.02, 0.03, 0.04 and 0.05) mol/L were used to show the percent degradation of 4-CP as a function of the irradiation time. The results are plotted in Fig.4. From this figure, it can be noticed that the degradation rate of 4-CP increased as the concentration of H_2O_2 increased from 0.02 to 0.03mol/L, and achieve 100% degradation at 0.03mol/L after 90 min of irradiation time. Then the degradation decreased as the H_2O_2 increased to 0.04 and 0.05 mol/L.

Fig.5 shows the degradation of 4-CP at different concentrations of H_2O_2 at irradiation time of 90 minutes .The percent of degradation increased to 100% at 0.03 mol/L of H_2O_2 then decreased to 45% at 0.05mol/L of H_2O_2 .

Investigators gave more than one explanation for these phenomena, among them:

-Hydroxyl radicals generated from the direct photolysis of hydrogen peroxide were the main responsible species of 4-CP elimination. It was expected that increasing the concentration of H_2O_2 reduces the rate of degradation of 4-CP, due to the reaction of hydrogen peroxide with these radicals, and hence acts as an inhibiting agent of 4-CP degradation (i.e. self-scavenging of OH by H_2O_2)

$$OH' + H_2O_2 \longrightarrow HO'_2 + H_2O$$
(4)

-Hydroxyl radical may recombine and participate in radical-radical reactions to form H_2O_2

$$2 \text{ OH}^{-} \longrightarrow H_2 O_2$$
 (5)

-At higher H_2O_2 concentrations there is lower light intensity available for 4-CP degradation, since H_2O_2 also absorb light in the system .This can possibly be attributed to low degradation of 4-CP.

-Hydroxyl radical efficiently reacts with H_2O_2 and produces HO_2° (equation 4). Since HO_2° radicals are not as reactive as OH^o, and then low degradation may be obtained. H_2O_2 is OH^o scavenger and so an excess H_2O_2 can result in a net decrease in the treatment efficiency (Kutschera et al., 2009).

However, if H_2O_2 dose is low, OH[•] formation will also be low, decreasing the treatment efficiency.

Yasmen A. Mustafa Ahmed H. Shihab

Therefore, a balance must be maintained between excess and low levels of H_2O_2 .



Fig. 4: Degradation of 4-CP by UV/H₂O₂ system, 4-CP= $0.39*10^{-3}$ mol /L, pH=3.The effect of initial H₂O₂ concentration.



Fig.5: Degradation of 4-CP as a function of H_2O_2 initial concentration by UV/ H_2O_2 system, 4-CP=0.39*10⁻³ mol/L, pH=3, irradiation time 90 min.

3.1.2. Reaction rate constant for UV/H₂O₂ system

The experimental data obtained for 4-CP degradation can be fitted according to a pseudo-first-order reaction as follows:

$$-\frac{dc}{dx} = KC \tag{6}$$

The integration leads to

$$\ln C/C_{o} = -K * t \tag{7}$$

where C_0 and C are the concentration of 4-CP at irradiation times 0 and t, K is a pseudo-first-order rate constant (in min⁻¹) and t is the irradiation

Removal of 4-Chlorophenoles from Simulated Wastewater by Advanced Oxidation Processes

time (in min). The regression analysis of the concentration curves versus reaction time indicates that the decomposition rate of this compound could be described by first order kinetics, Fig.6. A high increase in K was observed for 0.03mol/L H_2O_2 (0.086 min⁻¹) compared with other concentrations, Fig. 7.

3.2 UV/H₂O₂/Fe⁺³ (photo-Fenton) systems

3.2.1.The effect of initial H_2O_2 concentration on UV/ H_2O_2 /Fe⁺³system

In the photo-Fenton system both $Fe^{+3}(Fe_2(SO_4)_3;7H_2O)$ and H_2O_2 were used to attain the desirable degradation. First Fe^{+3} is fixed at constant concentration while H_2O_2 changed until high degradation was obtained.



Fig.6: Pseudo-first-order rate constant for 4-CP degradation by UV/H_2O_2 system, 4-CP=0.39*10⁻³ mol/L, pH=3.



Fig.7: Pseudo-first-order rate constant for 4-CP degradation as a function of H_2O_2 initial concentration by UV/ H_2O_2 system, 4-CP = $0.39*10^{-3}$ mol/L, pH=3, irradiation time 90 min.



Number 10

Volume 18 October 2012

In this sense, a series of experiments were carried out in order to determine the optimum ratio of H₂O₂/4-CP. Different concentrations of H₂O₂ (0.003, 0.004, 0.005, 0.006 and 0.007 mol/L) were used in the presence of fixed Fe^{+3} concentration 0.078×10^{-3} mol/L . H₂O₂/4-CP ratios for these concentrations were 8,10,13,15 and18 respectively, while the ratio of Fe⁺³/4-CP was 0.2. The results are plotted in Figs. 8 and 9. From these figures it can be noticed that a significant enhancement of degradation efficiency was observed when the H₂O₂ concentration was increased to 0.005 mol/L. (i.e. the ratio of $H_2O_2/4$ -CP = 13). Above this concentration, the oxidation rate seems to be negatively affected by the increase of H₂O₂ up to 0.007 mol/L (i.e. the molar ratio of $H_2O_2/4$ -CP =18). This is due to both the autodecomposition of H₂O₂ into oxygen and water, and the scavenging effect of hydroxyl radicals by H₂O₂. Excess of H₂O₂ will react with HO[•] competing with organic pollutants and consequently reducing the efficiency of the treatment.



Fig.8: Degradation of 4-CP by UV/H₂O₂/Fe⁺³ system, Fe⁺³ = $0.078*10^{-1}$ mol/L , 4-CP = $0.39*10^{-1}$ mol/L (Fe⁺³/4-CP=0.2) , pH=3.The effect of initial H₂O₂ concentration.



Fig.9:Degradation of 4-CP as a function of H_2O_2 initial concentration by UV/ H_2O_2 /Fe⁺³system, Fe⁺³=0.078*10⁻³ mol/L ,4CP=0.39*10⁻³ mol/L(Fe⁺³ /4-CP= 0.2), pH=3, irradiation time 30 min.

3.2.2. Reaction rate constant for UV/H₂O₂/Fe⁺³ system at constant Fe⁺³

The experimental data obtained for 4-CP degradation can be fitted according to a pseudo-first-order reaction; the results are plotted in Figs. 10 and 11. From these results it can be observed that addition of Fe⁺³ to UV/ H₂O₂ system with ratio of H₂O₂/Fe⁺³/4-CP equal to 13/0.2/1 enhanced the rate of 4-CP degradation by a factor of 1.9 (from 0.086 to 0.164 min⁻¹) and decrease the amount of H₂O₂ by a factor of 6 (from 0.03 to 0.005 mol/L).



Fig.10:Pseudo-first-order rate constant for 4-CP degradation by $UV/H_2O_2/Fe^{+3}$ system $Fe^{+3}=0.078*10^{-1}$ mol/L, 4-CP = $0.39*10^{-1}$ mol/L (Fe⁺³ /4-CP= 0.2), pH=3.



Fig.11:Pseudo-first-order rate constantfor4-CP degradation as a function of H_2O_2 initial concentration by UV/ H_2O_2 /Fe⁺³ system,4-CP=0.39*10⁻¹ mol/L ,Fe⁺³ =0.078*10⁻¹ mol/L (Fe⁺³/4CP=0.2),pH=3,irradiation time=30min.

3.2.3.Effect of using Fe^{+2} or Fe^{+3} onUV/H₂O₂/Fe⁺³ system

Iron in its ferrous Fe⁺² (FeSO₄.7H₂O) and ferric Fe⁺³ (Fe₂(SO₄)₃.7H₂O) form was used as photocatalyst in the photo-Fenton system. with 4-CP concentration Experiments of $0.39*10^{-3}$ mol/L, H₂O₂ of 0.005 mol/L, Fe⁺² or Fe^{+3} of 0.078*10⁻³mol/L and pH =3 were carried out in order to study the influence of using Fe^{+2} or Fe^{+3} on the degradation process. The results are plotted in Fig. 12. It can be seen from this figure, a slight increase in degradation was obtained for Fe⁺³ photocatalyst. This may be illustrated as, the Fenton process is carried out in presence of Fe^{+2} as catalyst; however the mineralization step appears to be driven by Fe⁺³ catalyzed processes, especially in the presence of light (Pignatello et al., 1999). In the light of the experimental results besides the fact that degradation appears to be driven by Fe^{+3} , Fe^{+3} has been selected as catalyst to be used in the photo-Fenton experiments.

3.2.4.The effect of initial Fe⁺³ concentration on UV/H₂O₂/Fe⁺³system

The effect of initial Fe^{+3} concentrations on photo-Fenton process was tested by carrying out experiments with various amounts of Fe^{+3} (0.04, 0.078, 0.16, 0.23 and 0.31)*10⁻³ mol/L. $Fe^{+3}/4$ -CP ratios for these concentrations were 0.1, 0.2, 0.4, 0.6 and 0.8 respectively. The optimum H₂O₂ concentration 0.005 mol/L (i.e. the ratio of H₂O₂/4-

Removal of 4-Chlorophenoles from Simulated Wastewater by Advanced Oxidation Processes

CP =13) was used in these experiments. The results are plotted in Figs. 13 and 14. From these figures it can be noticed that the addition of Fe⁺³ enhanced the efficiency of UV/H₂O₂ system for 4-CP degradation. The degradation rate of 4-CP distinctly increased with increasing amounts of the iron salt. It reached its maximum value at $0.16*10^{-3}$ mol/L Fe⁺³ (Fe⁺³/4-CP ratio =0.4) after about 10min of irradiation time. The addition of the iron salt above this value did not affect the degradation, and had a negative effect.



Fig.12:The effect of Fe⁺² and Fe⁺³on the 4-CP degradation by UV/H₂O₂/Fe system, 4-CP= $0.39*10^{-3}$ mol/L, H₂O₂= 0.005 mol/L (H₂O₂/4-CP=13), Fe⁺² = Fe⁺³ = 0.078*10-3 mol/L (Fe/4-CP=0.2), pH=3.



Fig.13: Degradation of 4-CP by UV/H₂O₂/Fe⁺³ system, H₂O₂=0.005mol/L ,4-CP = $0.39*10^{-3}$ mol/L (H₂O₂/4-CP=13), pH=3.The effect of initial Fe⁺³concentration.





Fig.14: Degradation of 4-CP as a function of Fe^{+3} initial concentration, $H_2O_2= 0.005 \text{ mol/L}$, $4\text{-CP}=0.39*10^{-3} \text{ mol/L}$ ($H_2O_2/4\text{-CP}=13$), pH=3, irradiation time 30 min.

3.2.5. Reaction rate constant for UV/H₂O₂/Fe⁺³ system at constant H₂O₂

The experimental results in Figs. 15 and 16 show that the reaction rate was of a first order and the photo-Fenton process had a significant accelerating effect on the rate of oxidation of 4-CP. The reaction rate constant reaches its maximum value at $0.16*10^{-3}$ mol/L Fe⁺³(i.e. H₂O₂/Fe⁺³/4-CP ratio =13/0.4/1). It can be observed that the photo-Fenton process enhanced the rate of 4-CP oxidation by a factor of 7 compared with UV/H₂O₂ system (i.e. K increased from 0.086 to 0.614 min⁻¹).

The optimum ratio for H_2O_2/Fe^{+3} /4-CP was 13/0.4/1 which represents a ratio of 31 for H_2O_2/Fe^{+3} . This result is in a good agreement with Kavitha and Palanivelu (2004), they reported that the optimal ratio was 20–40 and also with Kuo and Wu (2010), they showed that the optimal ratio of H_2O_2/Fe^{+3} was 40.

3.3.Effect of the pH value on $UV/H_2O_2/Fe^{+3}$ system

The photo-Fenton reaction is strongly affected by the pH-dependence. The pH value influences the generation of OH radicals and thus the oxidation efficiency. Different values of pH (2, 3, 4 and 5) were used to show its influence on the degradation of 4-CP. The results are plotted in Figs. 17 and 18. From these figures, it can be noticed that the maximum degradation was obtained with the system $UV/H_2O_2/Fe^{+3}$ at pH=3. For pH values above 3 the degradation strongly decreases, that is because at higher pH values iron precipitates as hydroxide and that reduces the transmission of the radiation. At lower levels of pH self-decomposition of hydrogen peroxide is promoted (Meric et al.,2004).

Therefore, a balance must be maintained to get an optimum condition. Figs. 19 and 20, illustrate the influence of pH values on the reaction rate of 4-CP.



Fig.15:Pseudo-first-order rate constant for 4-CP degradation by $UV/H_2O_2/Fe^{+3}$ system, $H_2O_2 = 0.005$ mol/L, 4-CP=0.39*10^{-‡}mol/L ($H_2O_2/4$ -CP=13), pH=3.



Fig.16:Pseudo-first-order rate constant for 4-CP degradation as a function of Fe⁺³ initial concentration by UV/H₂O₂/Fe⁺³ system, H₂O =0.005 mol/L, 4- CP=0.39* mol/L (H₂O₂/4-CP=13), pH=3, irradiation time 30 min.



Fig.17: Degradation of 4-CP at different pH values by UV/H₂O₂/Fe⁺³ system, Fe⁺³=0.16*10⁻¹mol/L, H₂O₂ = 0.005 mol/L, 4-CP=0.39*10⁻¹mol/L.

Yasmen A. Mustafa Ahmed H. Shihab



Fig.18: Degradation of 4-CP as a function of pH values by $UV/H_2O_2/Fe^{+3}$ system, $Fe^{+3} = 0.16*10^{-3}$ mol/L, H_2O_2 =0.005mol/L,4CP=0.39*10⁻³ mol/L, irradiation time 20 min.



Fig.19:Pseudo-first-order rate constant for 4-CP degradation by UV/H₂O₂/Fe⁺³ system at different values of pH, Fe⁺³= $0.16*10^{-3}$ mol/L, H₂O₂=0.005 mol/L, 4-CP= $0.39*10^{-3}$ mol/L.



Fig.20:Pseudo-first-order rate constant for 4-CP degradation by UV/H₂O₂/Fe⁺³system as a function of pH, Fe⁺³=0.16*10⁻¹mol/L, H₂O₂=0.005 mol/L, 4-CP=0.39*10⁻¹mol/L, irradiation time 20 min.

3.4. Effect of initial 4-CP concentration on $UV/H_2O_2/Fe^{+3}$ system

Experiments with 10ppm (0.078 $*10^{-3}$ mol/L) and 100ppm (0.78 $*10^{-3}$ mol/L) of 4-CP in the UV/H₂O₂/Fe⁺³ system were performed to see the

Removal of 4-Chlorophenoles from Simulated Wastewater by Advanced Oxidation Processes

effect of initial concentration change on the degradation process. Figs. 21 and 22, show the UV-vis spectra for 4-CP degradation and its products at different irradiation time at 10 and 100ppm respectively. Referring to Figs. 21A and B, a high powerful oxidization ability for photo-Fenton system toward low level concentration of 4-CP (10ppm) was observed.

No absorbance in the region of intermediate degradation products was observed for hydroquinone (221 and 290 nm) and benzoquinone (247 and 500nm). After only 5 min of irradiation time a complete degradation of 4-CP was observed. Referring to Figs. 22A and B, for high 4-CP concentration (100ppm), a gradual rise in the base line over time was observed .The base line reached a maximum and then tended to decrease gradually for longer irradiation times. This can be the result of the accumulation of degradation products such as hydroquinone which absorb light at about the same wavelength range (221 and 290) nm as 4-CP and benzoquinone (at 247nm). In the visible spectrum, the signal of benzoquinone (at 500nm) is small, but it can be observed at all the times of the experiment.



Fig.21(A and B): UV-visible spectra for 4-CP degradation by UV/ H_2O_2/Fe^{+3} system , $Fe^{+3} = 0.16*10^{-3}$ mol/L , $H_2O_2 = 0.005, 4$ -CP= 0.078 *10⁻³ mol/L (10ppm), pH=3, irradiation time 30min.

Number 10 V

Volume 18 October 2012



Fig.22(A and B): UV-visible spectra for 4-CP degradation by UV/H₂O₂/Fe⁺³system, Fe⁺³= 0.16 * 10^{-3}

mol/L, $H_2O_2 = 0.005$ mol/L, 4-CP= 0.78 *10⁻³ mol/L (100ppm), pH= 3, irradiation time 30 min.

3.5. Evolution of color due to intermediate formation

The main intermediates that were generated during the 4-CP degradation are hydroquinone and benzoquinone. Hydroquinone was the primary formed product from the degradation of 4-CP .A colored solution of benzoquinon could be observed through the first 5 minutes of irradiation time for UV/H₂O₂ system when low concentration (0.01 mol/L) of H_2O_2 was used. This can be indicated from the absorption peaks that appear at 500nm, Fig.23. The initial colorless of the solution became green in first 5 minutes of reaction and then dark green after 15 minutes, and gradually the color intensity decreased, finally disappeared, Fig 24. Also the colored solution of benzoquinone could be observed through the first 5 min for the $UV/H_2O_2/Fe^{+3}$ system at high concentration (100ppm) of 4-CP. It can realized that when there is insufficient amount of reagents required to degraded the 4-CP ,intermediate compounds from the degradation product were formed and remain in the

solution where longer irradiation time for complete degradation and mineralization of 4-CP is required.

3.6. Comparison between UV/H_2O_2 and $UV//H_2O_2/Fe^{+3}$ systems

The photo degradation of 4-CP was investigated in both systems UV/H₂O₂ and photo-Fenton UV /H₂O₂/Fe⁺³. The optimum results are listed in Table 3. It can be indicated that the photo-Fenton system had a significant accelerating effect on the rate of oxidation of 4-CP. The data in Table 3 show that adding Fe⁺³ to the UV/H₂O₂ system enhanced the rate of 4-CP oxidation by a factor of 7, reduce the consumption of H₂O₂ by a factor of 6 and the irradiation time required for complete degradation was reduced by a factor of 6. The intermediate products were also minimized.



Fig.23:UV-visible spectra for the 4-CP degradation and its photoproducts, $4\text{-CP} = 0.39*10^{-3}\text{mol/L}$, $H_2O_2=0.01 \text{ mol/L}$, pH= 3.



Fig.24: Closer photos inside the reactor for the color evolution in 4-CP solution, $H_2O_2 = 0.01 \text{ mol/L}, 4\text{-CP} = 0.39*10^{-3} \text{ mol/L}, \text{pH=3}$, irradiation time 120 min.

Table 3

System	H ₂ O ₂ (mol/L)	Fe ⁺³ (mol/L)	р Н	Irradiation time(min)	K (min- ¹)
UV/H ₂ O ₂	0.03		3	90	0.086
$UV/H_2O_2/Fe^{+3}$	0.005	0.16*10 ⁻³	3	15	0.614

4. Conclusions

The main conclusions that can be drawn from the experimental work of this study are as follows:

1. When there is insufficient amount of reagents required to degrade 4-CP, intermediate compounds from the degradation product are formed, remain in the solution and need longer irradiation time for complete degradation and mineralization. The intermediate products are identified:

- At low concentration of H_2O_2 (0.01mol/L) in UV/ H_2O_2 system for 4-CP at concentration of 50ppm.

- At high concentration of 4-CP (100ppm) for $UV/H_2O_2/Fe^{+3}$ system at H_2O_2 concentration of 0.005mol/L.

2. When insufficient amounts of reagents are used, a colored substance (benzquinone) was formed in the above systems (smaller signal of benzquinone for $UV/H_2O_2/Fe^{+3}$ system) after 5 min of irradiation time then the color intensity are decreased and disappeared at longer irradiation time ,120mim for UV/H_2O_2 and 30min in $UV/H_2O_2/Fe^{+3}$ systems.

3. The study showed that the photo-Fenton process, was the most effective treatment process under acidic conditions pH=3 and produced a higher rate of degradation of 4-CP at a short irradiation time. The results show that adding Fe⁺³ to the UV/H₂O₂ system with a molar ratio of H₂O₂/Fe⁺³/4-CP equal to 13/0.4/1 enhanced the rate of 4-CP oxidation by a factor of 7, reduce the consumption of H₂O₂ by a factor of 6 and the irradiation time required to complete degradation was reduced by a factor of 4.5. The intermediate and colored products were also minimized.

4. The experimental results showed that the optimum reagents for a complete degradation of 4-CP (50ppm) were obtained at pH=3, H₂O₂=0.005 mol/L, Fe⁺³ =0.016 mol/L and irradiation time of

Removal of 4-Chlorophenoles from Simulated Wastewater by Advanced Oxidation Processes

15 min for UV/H₂O₂/Fe⁺³ system with a molar ratio of H₂O₂/Fe⁺³/4-CP equal to 13/0.4/1.

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Number 10

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