DEVELOPING A COMPUTER PROGRAM FOR MODELING THE STADIA MEASUREMENTS FOR TACHEOMETRY WORKS

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ABSTRACT: Tacheometry is used to measure the lengths of traverse sides, to check the more accurate taped distances in order to uncover gross errors or mistakes and to determine differences of elevation between points. It's most general use is found in the compilation of planimetric and topographic maps by field methods alone, by which distances, elevations and directions to points are to be determined from field control points whose positions have been established by a higher order of accuracy.

The principles of stadia measurement by use of the transit or theodolite or total station is one of the main method of tacheometry. This paper presents the principles of stadia measurement and a computer program **MSM** (<u>M</u>odeling the <u>S</u>tadia <u>M</u>easurements). The program is formulated and written by using the Visual Basic language, Version 6. This version of the language is objecting oriented provided with comprehensive tools to simplify the task of programming and to provide the programmer with wide range of options for design of the user interface system.

التاكيوميتري يستعمل لقياس اطوال اضلاع المضلع, لتدقيق المسافات المسجلة والاكثر دقة لكي تكشف الاخطاء الاجمالية وتعيين اختلاف الارتفاعات بين النقاط. ويعتبر استعمال عام جدا في تجميع الخرائط البلانمترية ,الخرائط الطبوغرافية بواسطة طرق الحقل لوحدها, عن طريق قياس المسافات, والارتفاعات, وقياس الاتجاهات الى النقاط وذلك لتعيين نقاط الضبط الارضى التي اسست بدقة عالية.

ان مبادىء طريقة الستيديا والتي تتم بأستخدام اجهزة الترانست او الثيودولايت او جهاز المحطة الكاملة (Total Station) (Instrument هي واحدة من الطرق الرئيسية للتاكيوميتري. ان هذا البحث يعرض مبادىء طريقة الستيديا وتم عمل برنامج حاسوب اسمه ((MSM)) Measurements (في العداد البرنامج بإستعمال لغة الفجوال بيسكِ، نسخة 6. هذه النسخة من اللغة موجهة ومجهزة بالأدوات الشاملة لتَبْسيط مهمّةِ البرمجة ولتَزويد المبرمج بتشكيلة واسعة من الخياراتِ لتصميم واجهات البرامج.



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الخلاصة:

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	works

Keyword:

Stadia Measurements, Measurement by stadia horizontal sights, Stadia Leveling, Applications of Stadia Measurement, Stadia Surveying, Horizontal Measurements Distances and Tacheometry.

1. INTRODUCTION

The term tacheometry in surveying is used to denote the procedures for obtaining horizontal distances and difference in elevation by rapid indirect methods. The procedure is sometimes referred to as stadia, optical distance measurement or telemetry [4].

The stadia method is a rapid and efficient way to measure distances accurately enough for trigonometric leveling, some traverse, and the location of topographic details. Furthermore, a two-or three-man party can replace the three-or four-man party required in transit-tape surveys. The term stadia comes from the Greek word for a unit of length originally applied in measuring distances for athletic contests. The word denoted 600 Greek feet, or 606 ft 9 in. by present-day American standards.

The term "Stadia" is now applied to the cross wires and rod used in making measurements, as well as to the stadia method itself. Stadia reading can be taken with modern transits, theodolites, levels, and Total Station [1].

2. BASIC PRINCIPLE:

Stadia is based on similar triangles between the object, the focal point of lens, and the reticle of the instrument. The relationship is shown in Figure (1).



then

If f/ab = K, then d = KI and the horizontal distance, D, from the instrument to the rod is:

 $D = KI + C \tag{2}$

3. MEASUREMENT BY STADIA FOR HORIZONTAL SIGHTS

The stadia method is based upon the principle that in similar triangles homologous sides are proportional. Thus in Figure (2), which shows an external-focusing telescope, light rays from points A and B passing through the center of the lens the form a pair of similar triangles AmB

and *amb*. Here Ab=R is the rod intercept (stadia interval) and ab is the interval between the stadia wires [4].

Standard symbols used in stadia measurements, and their definition, are as follows:

 $f = focal \ length$ of the lens (a constant for any particular compound objective lens). It can be determined by focusing upon a distant object and measuring the distance between the center (actually the *nodal point*) of the objective lens and the reticle.

fI = distance from the center (actually the nodal point) of the objective lens to the plane of the cross hairs when the telescope is focused on some definite point.

 f^2 = distance from the center (actually the nodal point) of the objective lens to definite point when the telescope is focused on that point. When f^2 is infinite, or very large, $f^1 = f^2$.

i = interval between the stadia wires (ab in figure (2)).

f/i = stadia interval factor, usually 100.

c= distance from the center of the instrument (spindle) to the center of the objective lens. It varies as the objective lens moves in and out for different sight lengths but is generally considered to be a constant [3].

C=*c*+*f*. C is called the stadia constant although it varies slightly with c.

d= distance from the focal point in front of the telescope to the face of the rod.

D = C + d = distance from the center of the instrument to the face of the rod.



Figure (2): Principle of stadia, external-focusing telescope.

4. INCLINED MEASUREMENT

When collecting measurements using stadia as presented earlier, the requirement of having horizontal sights is limiting in normal terrain. Thus, the stadia formulas need to be developed for inclined measurements. In Figure (3), the geometric relationships of an inclined stadia measurement can be seen. In this figure, the desired position of the rod is perpendicular to the line of sight as shown by r'. Since it is impractical in the field to hold the rod in this manner, a correction to the readings on the level rod r must be determined. From simple geometric relationships, it can be shown that the altitude angle of the line of sight, α , is the same as the angle between positions of r' and r. For small vertical angles, we can make the assumption that the angle at the intersection of the upper wire line of sight and r' is 90°, and thus a simple right triangle relationship can be developed between the reading on the rod r and the corrected reading on the rod r' as :

Making this correction to Equation (1), the slope distance between the instrument and the rod is [4]:

 $S = KI\cos(\alpha) + C \qquad (4)$

The Equation (3) can now be used to compute the horizontal distance between the instrument and the rod as [5]:

 $H = KI\cos^2(\alpha) + C \qquad(5)$

Since theodolites and total stations read zenith angles, we can use the trigonometric relationships of sin (a) = $\cos (90\text{-}a)$ to derive a similar equation for zenith angle reading instruments as:

 $H = KI\sin^2(z) + C \tag{6}$

where z is the zenith angle of the line of sight. Similarly an equation for computing V is:

 $V = KI \cos(\alpha) \sin(\alpha) = KI \cos(z) \sin(z) \qquad (7)$

Note that in Equation (6), the term $C \sin(\alpha)$, or alternatively $C \cos(z)$ has been dropped since for small altitude angle or large zenith angles the value of the trigonometric functions is very small, and thus so is their product with C [4].

Using Equations (2) and (6), an expression for the elevation difference between ground at the instrument station and at the rod can be derived as [5]:

 $\Delta Elev = hi + V - MW \dots (8)$



Figure (3): Inclined stadia measurement.

4.1 STADIA TRAVERSES

In a transit-stadia traverse, distances, horizontal angles, and vertical angles are measured at each corner. Reduction of stadia notes as the survey progresses provides elevations to be carried from hub to hub. Average values of stadia distances and differences in elevation are obtained from a foresight and a backsight on each line. An elevation check should be secured by closing on the initial point, or on bench marks near both ends for an open traverse [1].

4.2 TOPOGRAPHY

The stadia method is most useful in locating numerous topographic details, both horizontally and vertically, by transit or plane table. I n urban areas, angle and distance readings can be taken faster than a notekeeper is able to record the measurements and prepare a sketch [4].

4.3 STADIA LEVELING

The stadia method is adaptable to trigonometric leveling. The h.i. is determined by sighting on a point of know elevation, or by setting the instrument over such a point and measuring the height of the horizontal axis above it with a stadia rod [2]. The elevation of any point can then be found by computation from the rod intercept and the vertical angle. If desirable a leveling circuit can be run to establish and check the elevations of two or more points [6].

5. PRECISION

A ratio of error of 1/500 can be obtained for a transit-stadia traverse run with ordinary care. Short sights, a long traverse, and careful work may give ratios up to 1/100. Errors in stadia work are usually the result of poor rod readings rather than incorrect angles. An error of 1 min in reading a vertical angle does not appreciably affect the horizontal distance. The same 1-min error produces a difference in elevation of less than 0.1 ft on a 300 ft sight for any vertical angle [4].

6. MODELING THE STADIA MEASUREMENT

The stadia measurement is modeled by Visual Basic language as software named **MSM** (<u>M</u>odeling the <u>S</u>tadia <u>M</u>easurements). The program is formulated and written by using Visual Basic, Version 6. This version of the language is objecting oriented provided with comprehensive tools to simplify the task of programming and to provide the programmer with wide range of options for design of the user interface system. Figure (4) shows the flowchart of this software.

The input data for each one of these forms and the link between these forms are described in the following sections with the aid of flowcharts, which provide description for the logic and the steps followed in the development of the program.

7. PROGRAM MENUS AND INPUT FORMS

In Visual Basic programming the term FORM is usually used to refer to the graphical area appeared on the screen, which is used to hold objects that may be fields or tables containing values, graphics or text boxes for input the required data values. The form interface is used because most people are familiar with paper form. These forms are written in such away to be are user friendly and allow the data input to the program interactively. When the program (MSM) is run, the user presented with the form shown in figure (5).

This form displays program name and version, if the user select "Traverse and Leveling" from the main program menu interface displayed on the screen. The main Form of (MSM) also contains the cases of plotting the traverse and the cases of the plotting profile, as shown in figure (5).

The cases of plotting the traverse are classified into eight cases (number of sides = (3), number of sides= (4), number of sides= (5), number of sides= (6), number of sides= (7), number of sides= (8)), as it is clear in figure (5) and the cases of plotting profile classified into five cases (number of stations = (3), number of stations = (4), number of stations = (5), number of stations = (5), number of stations = (6), number of stations = (7), as shown in figure (6).









Figure (5): The main page of (MSM).



Figure (6): The main page of Leveling.

7.1 TRAVERSING

Traversing design is described in eight cases of the following:

1. Case1: number of sides = (3).

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- 2. Case2: number of sides = (4).
- 3. Case3: number of sides = (5).
- 4. Case4: number of sides = (6).
- 5. Case5: number of sides = (7).
- 6. Case6: number of sides = (8).
- 7. Case7: number of sides = (9).
- 8. Case8: number of sides = (10).

These menu items are described in the following sections.

Case1: number of Sides = (3)

If the user selects this option, the form shown in figure (5) is displayed on the screen. First the user input information's the requirements of the first traverse and is listed below:

- 1. Points of traverse (P1, P2, P3,).
- 2. The sides of traverse (L1, L2, L3).
- 3. Lengths of sides (S1 S2, S3).
- 4. Known coordinates (EP1, NP1), Height Instrument (HI), Constant (K), Elevation of first point (Elev.p1) and Midhair.
- 5. The Azimuth of sides (Az1, Az2, Az3).
- 6. The Vertical angles (Vangle1, Vangle2, Vangle3)

When the user input the required data as displayed in figure (7/a), the program begins the calculation of the elements (Horizontal Distance for each side, Vertical Distance for each side, Difference in Elevation for each side, Adjusted Elevation of the Traverse Stations, Departure of Sides, Sum of Departures, Latitude of Sides, Sum of Latitudes, Total Correction for Departures and Latitudes, Correction for Departure and Latitude for each meter from Length of Sides, Correction for Departures, Corrected Latitudes, Sum Corrected Departures, Sum Corrected Departures, Sum Corrected Departures, Sum Corrected Latitudes and Adjusted Coordinates (Easting and Northing of Points)) as shown in figure (7/b).

Traverse	(3 sides)									
Input					Output				Martin Control of Control of Control	
Pointe	ofTraverse	The Side	s of Travers		Horizontal E	listance for each side	Total Correct	ion for Departures and Latitudes	Adjusted Coordina North	ates (Easting and ding)
12		1.2	-		Hdistance1 Hdistance2		TCDeps		CorrEP2	
19		1.3			Hdistance3		TCLass	and the second	CorrErs	
Lengt	he of Sides	к	nowna		SumHdistances	•	for each mete	r from Longth of sides	CorrEP1	Check
NI I	m	10	1		Vertical Di	stance for each side	KD	1	CorrNP2	
N2 [m	к			Alphal		KL.		Correcto	1 44 4
83	m	Midhair	-		Alpha2		Correctio	a for Departures	Corrept	Check
		ElevPl	í —	m	AlphaJ		CorrforDep1			
Fenown	Coordinates		16		Difference in	Elevation for each side	CorrforDep2			
in i					DEI	Particular and a second s	CorrforDep3			
Part			_		DE2		Correcti	on for Latitudes		
	The Azimu	th of Sides			DID		CorrforLatl			
Avi	deg	min	Nest		Adjusted Elev	ation of the Traverse	CorrforLat2			
A42	deg	min	800			Matton	CorriorLati			
A23	deg	min	600		AdjElevP2		Correc	ted Departures		
	The Vertie	al angles			AdjElevP3	Loop of the	CorrDep1			
Vangle I	deg	min	Nec		AdjElevPl	Check	CorrDep2			
Vangle2	deg	min			Depa	cture of Sides	CorrDep3			
Vangle 3	deg	min			Depi		SumCorrDeps			
					Dep2		Corre	cied Latitudes		
	Calcu	dation			Deps		CorrLatl			
	- C				numbeps		CorrLat2			
	ante I	NI			Lati	fude of Sides	CorrLati			
	aca				Lati		SumCorrLats			
	Plotting T	raverse			Latz					
	81 mm	-	1		Laty	1				
	Sav	-			NumLate	1				

Figure (7/a): Traverse (3 Sides).

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🖻 Trav	verse (3 sides	s)										
Input	;					Output						
P	oints of Traver	rse	The Sid	es of Travers	æ	Horizontal	Distance for each side	Total Correcti	on for Departures and	Adjusted Coo	rdinates (H	Casting and
Pl	Α		Ll	AB		Hdistance l	324.957174152038		Latitudes	r	orthing)	
P2	В	_	L2	BC		Hdistance2	621.186758317448	TCDeps	28.1053191848234	CorrEP2	531.2100	069725095
P3	С	_	L3	CA	-	Hdistance3	508.272472028533	TCLats	-598.257652579774	CorrEP3	698.3967	794028879
	oughe of Sid		L			SumHdistanc	s 1454.41640449802	Correction for	Departure and Latitude	CorrEP1	200	Check
61			п		-	Vertical D	istance for each side	VD	I control the test	CorrNP2	70.49160	011597747
51	3.27		TL I	1.52	.	Alphal	25.76491635613	KD	1.93241214124807E-C	CorrNP3	416.4643	368307102
52	6.24	m	K	100		Alpha2	41.8036898030274	KL	J-0.411338630896602	CorrNP1	200	Check
\$3	5.09	m	Midhair	1.52		Alpha3	-19 2297280409172	Correctio	n for Departures			
K	nown Coordina	ates	ElevPl	300	m	Difference in	Elevation for each side	CorrforDep1	6.27951188717063			
EPI	200	_				DEI		CorrforDep2	12.0038883375517			
NPI	200	_				DE	41,000000000074	CorrforDep3	9.82191896010107			
	Th	ie Azimuť	h of Sides			DE2	41.8036898030274	Correcti	on for Latitudes			
Azl	89	16	. 00	_		DES	-19.2297280409172	CorrforLatl	-133.667439115728			
Az2	14 de	28	. 00	sec		Adjusted El	station of the Traverse	CorrforLat2	-255.518110697398			
Az3	269 de	g	min 👓	sec		AdiElevP2	325 76491635613	CorrforLat3	-209.072102766648			
	de de	g 10	min 👓	sec		AdiElevP3	367 569606159157	Correct	ted Departures			
	T	he Vertic:	al angles			AdiFlevPl	249 Check	CorrDep1	331.210069725095			
Van	glel +4	deg 32	min	00 sec		Den	orture of Sides	CorrDep2	167.186724303783			
Van	gle2 +3	deg 51	min	00 sec		Depl		CorrDep3	-498.396794028879			
Van	gle3 -2	deg 10	min	00 sec		Dep1	324.930557837925	SumCorrDeps	0			
						Dep2	155.182835966232	Correc	ted Latitudes			
		Calcu	lation			Dep3	-508.21871298898	CorrLatl	-129 508398840225			
						SumDeps	-28.1053191848234	CorrLat2	345 972767147327			
		1				La	titude of Sides	CorrLat3	216 464269207102			
	васк		N	ext		Latl	4.15904027550286	SumCorrLats	0			
	Plot	ting Tı	raverse			Lat2	601.490877844725	Suncomats	Jo			
	1100					Lat3	-7.39226554045352					
		Save	e			SumLats	598.257652579774					

Figure (7/b): Traverse (3 Sides) Input and Computation [4].

The results of all elements (Horizontal Distance for each side, Vertical Distance for each side, Difference in Elevation for each side, Adjusted Elevation of the Traverse Stations, Departure of Sides, Sum of Departures, Latitude of Sides, Sum of Latitudes, Total Correction for Departures and Latitudes, Correction for Departure and Latitude for each meter from Length of Sides, Correction for Departures, Corrected Latitudes, Sum Corrected Departures, Sum Corrected Departures, Sum Corrected Departures, Sum Corrected Latitudes and Adjusted Coordinates (Easting and Northing of Points)) are saved in a text file as shown figure (7/c). Following that the transition traverse design process is considered completed the program enabled the user to go to the design of the next traverse in the alignment irrespective of its case (3 sides or 4 sides or 5 sides or 6 sides or 7 sides or 8 sides or 9 sides or 10 sides) or can exit the traverse design if it is the last traverse in the alignment.

File Menu

The menu items available under the file menu are **Open**, **Save as, Save, Close, Print**, and **Exit**.

• When "**Open**" is selected, an existing design text file can be selected to open and made available to the user for seeing the calculated results or edit an existing file as shown in figure (7/d).

• When "Save As" is selected, a new file is created. The current file is then copied to the new file on the disk or location specified by the user.

• When **"Save"** is selected, an edited open file can be saved at any existing disk drive as shown in Figure (7/e).

- When "Close" is selected, to close opened text file.
- When "**Print**" is selected, to print text file.

• When "**Exit**" is selected, the program terminates, and the user is returned to the operating system level.

S Form26	
file Edit Format	
Form26 File Edit Format Horizontal Distance for each side Hdistance one =324.957174152038 Hdistance two =521.186756817448 Hdistance two =621.186756817448 Hdistance two =621.186756817448 Hdistance three=504.872225958399 Vertical Distance for each side Alpha two =41.8036898030274 Alpha two =41.8036898030274 Alpha three=-45.650832069486 Difference in Elevation for each side DE one =25.76491635613 DE two =41.8036898030274 DE bree=-45.650832069486 De one =25.76491635613 DE one =25.76491635613 De two =41.803689030274 DE bree=-45.650832069486 De parture on = =324.930557837925 Departure one =324.930557837925 Departure of Side Departure one =324.93057837925 Departure two = 501.488265565866 SumDeparture wo =501.490877644725 Latitude two = 501.490877644725 Latitude wo =501.490877647255 Latitude two = 501.490877644725 Latitude wo =501.490877644725 Latitude wo =501.490877644725 Latitude wo =501.490877644725 Latitude wo =501.490877644725 Latitude wo =501.490877644725 Latitude wo =501.490877644725 Latitude wo =501.490877644725	
Correction for Departures and Latitudes for each meter from Length of Sides KD =1.70262974736248E-02	
Correction for Departures	
CorrforDep1 = 6.53281751330111 CorrforDep2 = 10.5755105337296	
ConforD ep3 =8.59610470533882	
Correction for Latitudes	
Control_at1 = -133.991744424058	
CorrforLat2 =-256.138051351769 CorrforLat3 =-208.177309653032	



Open						17 🔀
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My Recent Documents Desktop						
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	File name:	1			-	Open
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Figure (7/d): Open file dialog box.

Save As						
Save in Mu Flavents Devictop My Documents My Documents My Computer	CPMSM		*	- 400 (SL)	c* m-	
	File name:	1			*	Save
My Network Places	Save as type:	Test Files(",T⊠T)			-	Cancel

Figure (7/e): Save file dialog box.

Case2: number of Sides = (4)

If the user selects this option, the form shown in figure (5) is displayed on the screen. First the user input information's the requirements of the second traverse and is listed below:

- 1. Points of traverse (P1, P2, P3, P4).
- 2. The Sides of traverse (L1, L2, L3, L4).
- 3. Lengths of sides (S1, S2, S3, S4).
- 4. Known coordinates (EP1, NP1), Height Instrument (HI), Constant (K), Elevation of first Point (Elev.p1), Midhair.
- 5. The Azimuth of sides (Az1, Az2, Az3, Az4).
- 6. The Vertical angles (Vangle1, Vangle2, Vangle3, Vangle4).

When the user input the required data as displayed in figure (8/a), the program begins the calculation of the elements (Horizontal Distance for each side, Vertical Distance for each side, Difference in Elevation for each side, Adjusted Elevation of the Traverse Stations, Departure of Sides, Sum of Departures, Latitude of Sides, Sum of Latitudes, Total Correction for Departures and Latitudes, Correction for Departure and Latitude for each meter from Length of Sides, Corrected Departures, Corrected Latitudes, Sum Corrected Departures, Sum Corrected Departures,

🖻 Traverse (4 sides)			
Input	Output		
Points of Traverse The Sides of Traverse	Horizontal Distance for each side	Latitude of Sides	CorrDep4
P1 L1	Hdistancel	Latl	SumCorrDeps
P2 L2	Hdistance2	Lat2	Corrected Latitudes
P3 L3	Hdistance3	Lat3	CorrLatl
P4 L4	Hdistance4	Lat4	CorrLat2
Lengths of Sides Knowns	SumHdistances	SumLats	CorrLat3
S1 m HI	Vertical Distance for each side	Total Correction for Departures and	CorrLa4
S2 m K	Alphal	Lannudes	SumCorrLats
S3 m Midhair	Alpha2	TCDeps	Adjusted Coordinates (Easting and
S4 m ElevPl m	Abha3	TCLats	Northing)
Known Coordinates	Alpha4	Correction for Departure and Latitude	CorrEP2
TDI	Difference in Elevation for each side	for each meter from Length of sides	CorrEP3
	DEI	KD	CorrEP4
	DEI	KL	CorrEP1 Check
The Azimuth of Sides	DE2	Correction for Departures	ComNP2
Azl deg min sec	DE3	CorrforDep1	ComNP2
Az2 deg min sec	DE4	CorrforDep2	ComNP4
Az3 deg min sec	Adjusted Elevation of the Traverse	CorrforDep3	ComNPl Check
Az4 deg min sec	ádiFlerP	CorrforDep4	Check
The Vertical angles	AdiFlerP3	Correction for Latitudes	
Vanglel deg min sec	AdiFlerP4	CorrforLatl	
Vangle2 deg min sec	AdiFlevPl	CorrforLat2	
Vangle3 deg min sec	Departure of Sides	CorrforLat3	Save
Vangle4 deg min sec	Den	CorrforLat4	
	Dep?	Corrected Departures	
	Dep1	CorrDep1	
Back Next	Dend	CorrDep2	
	SumDens	CorrDep3	
Plotting Traverse			

Figure (8/a): Traverse (4 Sides).

The result of all elements (Horizontal Distance for each side, Vertical Distance for each side, Difference in Elevation for each side, Adjusted Elevation of the Traverse Stations, Departure

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of Sides, Sum of Departures, Latitude of Sides, Sum of Latitudes, Total Correction for Departures and Latitudes, Correction for Departure and Latitude for each meter from Length of Sides, Correction for Departures, Correction for Latitudes, Sum Corrected Departures and Latitudes, Corrected Departures, Corrected Latitudes, Sum Corrected Departures, Sum Corrected Latitudes and Adjusted Coordinates (Easting and Northing of Points)) are saved in a text file. Following that the transition traverse design process is considered completed the program enabled the user to go to the design of the next traverse in the alignment irrespective of its case (3 sides or 4 sides or 5 sides or 6 sides or 7 sides or 8 sides or 9 sides or 10 sides) or can exit the traverse design if it is the last traverse in the alignment.

🗟 Travers	se (4 sides)										
Input						Output					
Poin	ts of Traverse	•	The Sid	les of Travers	e	Horizontal D	istance for each side	Latit	tude of Sides	CorrDep4	28.0923684243377
Pl	Α		Ll	AB		Hdistance l	324.957174152038	Latl	4.15904027550286	SumCorrDeps	0
P2	В		L2	BC		Hdistance2	621.186758317448	Lat2	601.490877844725	Correc	ted Latitudes
P3	С		L3	CD		Hdistance3	505.03005174651	Lat3	-7.34510809432466	CorrLatl	5.91060497994983
P4	D		L4	DA		Hdistance4	610.126680568631	Lat4	-609.415509456101	CorrLat2	604.839161518036
Len	igths of Sides]	Knowns		SumHdistances	2061.30066478463	SumLats	-11.1106994301981	CorrLat3	-4.62292534629787
S1	3.27	m	Ш	1.52	[Vertical Dis	stance for each side	Total Correctio	on for Departures and	CorrLa4	-606.126841151688
S2	6.24	m	К	100		Alphal	25.76491635613	L	atitudes	SumCorrLats	0
S 3	5.09	m	Midhair	1.52		Alpha2	41.8036898030274	TCDeps	-4.58676963045401	Adjusted Coor	dinates (Easting and
S4	6.11	m	ElevPl	300	m	Alpha3	-44.7765917851198	TCLats	11.1106994301981	N	orthing)
Кноч	vn Coordinate	s				Alpha4	-23.0832295343819	Correction for for each mete	Departure and Latitude r from Length of sides	CorrEP2	524.207468905261
EPI	200					Difference in I	Elevation for each side	KD	-2 22518223993939E-	CorrEP3	678.008051129199
NP1	200					DE1	25.76491635613	KL	5 3901401285188E-01	CorrEP4	171.907631575662
	The	Azimut	th of Sides			DE2	41.8036898030274	Correctio	n for Departures	CorrEP1	200 Check
Azl	89 deg	16	min 00	sec		DE3	-44.7765917851198	CorrforDenl	.0.723088932664006	CortNP2	205.91060497995
Az2	14 deg	28	min 00	sec		DE4	-23.0832295343819	CorrforDep2	1 38225374229351	CorrNP3	810.749766497986
Az3	269 deg	10	min 00	sec		Adjusted Elev	ation of the Traverse	CorrforDep3	1123783901782	CorrNP4	806.126841151688
Az4	177 deg	14	min 00	sec			station	CorrforDep4	1.125764305371449	CortNP1	200 Check
	The	Vertic	al angles			AdjElevP2	325.76491635613	Correcti	on for Latitudes		
Vangle	1 +4 -	32		00		AdjElevP3	367.568606159157	CorrforLatl	1 75156470444698		
Vangle	2 +3	eg 📴	min	sec		AdjElevP4	322.792014374038	CorrforLat2	3 34828367331139		
Vangle	3 <u>5</u>	eg 📫	<u></u> тин	sec		AdjElevPl	300 Check	CorrforLat3	2 72218274802679		Save
Vangle ⁴	4 <u>-</u> 2 .	eg 🔽	- min	sec		Depar	ture of Sides	CorrforLat4	3 28866830441295		
		eg 📫	' min	sec		Dep1	324.930557837925	Correct	ted Departures		
		Calc	ulation)		Dep2	155.182835966232	CorrDep1	324 207468905261		
	Back	1		Nevt	1	Dep3	-504.976635651754	CorrDep2	153 800582223938		
	Datk		_	INCAL	_	Dep4	29.4500114780522	CorrDep3	-506 100419553536		
	Ple	otting	g Trave	erse		SumDeps	4.58676963045401	como cho	1 000,10041000000		

Figure (8/b): Traverse (4 Sides) Input and Computation [4].

Plotting Traverse

When this option is selected the figure shown in (8/b) presented to the user. The user has to input the following information:

- Corrected Easting of points (EP1, CorrEp2, and CorrEp3,.....).
- Corrected Northing of points (NP1, CorrNp2, and CorrNp3,.....).
- Scale (S).

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When these data are input the computer program and when the user selects "**plotting traverse**" button to begin by drawing the points are illustrated in the below figures (9/a),(9/b),(9/c),(9/d),(9/e),(9/f),(9/g) and figure (9/h). The program output result is saved for later use by the user in a text file.

Correcte	d Easting of Fonits	Corrected	reording of Folics	Scale
EP 1	1000	NP1	1000	Xmax 1500
CorrEP2	1306.985	CorrNP2	1558.998	Ymax 1200
CorrEP3	897.694	CorrNP3	1272.898	

Figure (9/a): Plotting Traverse (3 points) Input and Plotting.

00110000	d Easting of Points	Corrected	l Northing of Points	s	cale
EP 1	1000	NP1	1000	Nmax	1500
CorrEP 2	1209.027	CorrNP2	1456.023	Ymax	1500
CorrEP3	607.896	CorrNP3	968.255		
CorrEP4	625.296	CorrNP4	606.103		
			/ ⁸		
	c		/"	Plotting T Ba	raverse ck

Figure (9/b): Plotting Traverse (4 points) Input and Plotting.

H Plotting T	TRANSPORTED IN	(5 Points)					\times
Cor	rected	Easting of Points	Corrected	Northing of Points	5	Scale	
RCF RCF	1	1000	NP1	1000	Nmax	1500	
Corr	-EP 2	1130.694	CorrNP2	1455.969	Ymax	1500	
Corr	1000 00	376.125	Corrrer.3	968.094		,	
Corr	- EEP - 4	325.621	CorrPIP-1	605.095			
Corr	EP 5	617.804	CorrNPS	1001.363			
			7	в			
					Plotting		
			/				
		E	/		в	ack	
			^				
'		ь					

Figure (9/c): Plotting Traverse (5 points) Input and Plotting.

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	rise (6 Points)			
Correcte	d Easting of Points	Corrected	I Northing of Points	Scale
EP 1	1000	NP 1	1000	Xmax [1600
CorrEP2	1146.444	CorrNP2	1421.990	Ymax 1600
CorrEP3	476.000	CorrNP3	867,369	
CorrEP4	454.757	CorrTVP4	475.694	
Corvers	701.015	Contrips	033.156	
CorrEP6	1194.015	CorrPIPS	900.736	
		1"		Back
	C E	- A		





Figure (9/e): Plotting Traverse (7 points) Input and Plotting.

			TT		1
correcte	d Easting of Points	Corrected	Northing of Points	6	cale
EP 1	1000	NP1	1000	Xmax	1750
torren e Par	1091.472	CorrNP2	1370.143	Ymax	1750
orrenter a	230.536	CorrNP3	714.189		
ora EP 4	137.376	CorrNP4	277.601		
orrEP.6	375.763	CorrNPS	579.719		
orrEPG	713.057	CorrNP6	500.047		
lossEP7	467.001	Com/NP7	667.328		
orrEP8	699.803	CorrNP8	1992.209		
c	0	^B		Plotting	Traverse ack

Figure (9/f): Plotting Traverse (8 points) Input and Plotting.



Figure (9/g): Plotting Traverse (9 points) Input and Plotting.



Figure (9/h): Plotting Traverse (10 points) Input and Plotting.

7.2 LEVELING

Leveling design is described in five cases of the following:

- 1. Case1: number of Stations = (3).
- 2. Case2: number of Stations = (4).
- 3. Case3: number of Stations = (5).
- 4. Case4: number of Stations = (6).
- 5. Case5: number of Stations = (7).

These menu items are described in the following sections.

Case1: number of Stations = (3)

If the user selects this option, the form shown in figure (6) is displayed on the screen. First the user input information's the requirements of the first leveling and is listed below:

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- 1. Stations (Sta1, Sta2), Rod (Rod1, Rod2) and Interval (S1, S2) for Backsight.
- 2. The Vertical angles (Vangle1, Vangle2) for Backsight.
- 3. Stations (Sta2, Sta3), Rod (Rod2, Rod3) and Interval (S2, S3) for Foresight.
- 4. The Vertical angles (Vangle2, Vangle3) for Foresight.
- 5. Known Elevation of point (TBM2) and Constant (K).

When the user input the required data as displayed in figure (10/a), the program begins the calculation of the elements (Vertical Distances for Backsight, Vertical Distances for Foresight, Elevation of the Stations, Backsight and Sum of Backsight, Foresight and Sum of Foresight, Height Instrument, Z, Q and N) as shown in figure (10/b).

Leveling (3 Stations)						
Input			Output			
Backsight	_	_	Vertical Distan	ces for Backsight	He	ight Instrument
Station Rod	Interval		Vdl	fi	HII	ft
Stal Rodl	ft Sl	ft	Vd2	fi	HI2	ft
Sta2 Rod2	ft S2	ft	Vertical Distan	ces for Foresight	Elev	vation of Stations
The Vertical angles			Vd2	fr	FlerTPl	ft
Vanglel dag win	597		Vd2	A	FlowTP?	
Vangle2	Sec		100	n	Elev I F2	
deg j min j	sec		Backsi	ght	F	oresight
Foresight	t	_	BS1	ft	FS2	fi
Station Rod	Interval		BS2	ft	FS3	ft
Sta2 Rod2	ft S2	ft	Sum BS	Check	Sum FS	Check
Sta3 Rod3	ft S3	ft			_	
The Vertical angles			Z = (SumBS - Su	nFS)		Check
			Q = Elev Final poin	t (TBM3) - Elev First P	oint (TBM2)	Check
deg min	sec		N = (Z - Q)			Check
Vangle3 deg min	sec					
Knowns						
К	Colculation		D	adr		Novt
ElevTBM2 ft			D	аск		INEXt
				DI-449	Durfla	
Save				Plotting	Prome	

Figure (10/a): Leveling (3 Stations).

The results of all elements (Vertical Distances for Backsight, Vertical Distances for Foresight, Elevation of the Stations, Backsight and Sum of Backsight, Foresight and Sum of Foresight, Height Instrument, Z, Q and N) are saved in a text file. Following that the transition leveling design process is considered completed the program enabled the user to go to the design of the next leveling in the alignment irrespective of its case (3 stations or 4 stations or 5 stations or 6 stations or 7 stations) or can exit the leveling design if it is the last leveling in the alignment.

		N	umber	2		Volume	15 Ju	ne 2009		Journ	al of Eng	gineering	
•													
🗟 Leveli	ng (3 Stations)											
Input								Output					
			Backsight	;	_			Vertical	Distances for Back	sight	He	ight Instrument	
\$	tation		Rod		_	Interval		Vdl	2.28339192868951	ft	HII	1410.48339192869	fi
Stal	TBM2	Rodl	8.6	ft	S1	3.14	ft	Vd2	35.7722155099583	fì	HI2	1463.09667832923	ft
Sta2	TP1	Rod2	4.5	ft	S2	6.32	ft	Vertical	Distances for Fores	sight	Elev	vation of Stations	
	The Vert	ical angl	es					Vd2	-15.0410708905804	ft	ElevTP1	1431.82446281927	ft
Vangle	1 +0 de;	g 25	min 00	sec				Vd3	-55.258213233242	ft	ElevTP2	1520.55489156247	fi
Vangle	2 +3 de;	g 15	min 00	sec					,				
		0	Foresig	nt				H	Backsight		F	oresight	
	Station		Rod			Interval		BSI	-6.31660807131049	fi	FS2	-21.3410708905804	ĥ
Sto?	TDI	Rod?	Kou	ft	\$2	Inter var	- ft	BS2	31.2722155099583	fi	FS3	-57.458213233242	ft
Stat.	IPI	Ded2	0.3		63	4.02		Sum BS	24.9556074386478 Ch	neck	Sum FS	-78.799284123822 Che	eck
514.5	IBM3	Kous	2.2	n	93	5.04	- "	Z = (SumE	S - SumFS)		10	03.75489156247 Check	
	The Ver	tical ang	gles					Q = Elev Fin	al point (TBM3) - Elev	First Point	t (TBM2)	3.75489156247 Check	
Vang	le2 -1 d	leg 52	min 00	sec				N = (Z - Q)			0	Check	
Vang	le3 -6 d	leg 20	min 00	sec							10		
	Knowns												
K	100	1							D I				
ElevTI	IM2 1416.8	ft			Ca	alculation	1	_	Back			Next	
												1	
			Save						Plot	tting P	rofile		
		_											

Figure (10/b): Leveling (3 Stations) Input and Computation [4].

Case2: number of Stations = (4)

100

If the user selects this option, the form shown in figure (6) is displayed on the screen. First the user input information's the requirements of the second leveling and is listed below:

1. Stations (Sta1, Sta2, Sta3), Rod (Rod1, Rod2, Rod3) and Interval (S1, S2, S3) for Backsight.

2. The Vertical angles (Vangle1, Vangle2, Vangle3) for Backsight.

3. Stations (Sta2, Sta3, Sta4), Rod (Rod2, Rod3, Rod4) and Interval (S2, S3, S4) for Foresight.

4. The Vertical angles (Vangle2, Vangle3, Vangle4) for Foresight.

5. Known Elevation of point (TBM2) and Constant (K).

When the user input the required data as displayed in figure (11/a), the program begins the calculation of the elements (Vertical Distances for Backsight, Vertical Distances for Foresight, Elevation of the Stations, Backsight and Sum of Backsight, Foresight and Sum of Foresight, Height Instrument, Z, Q and N) as shown in figure (11/b).

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out		10.4.5		Output			
	Backsig	ut.		Vertical Distan	ces for Backsight	He	ight Instrument
Station	Rod	Inte	rval	Vd1	n	нп	n
ital	Rod1	S1	ft	Vd2	ft	HI2	R
ita2	Rod2	S2	n (Vd3	ñ	ню	n
ita3	Rod3	S 3	fi	Vertical Distan	ces for Foresight	Elev	vation of Stations
The V	/ertical angles			Vd2	1	ElevTP1	1
angle 1	deg min	sec		Vd3	n	ElevTP2	1
angle2	dog min	sec		Vd4	n	ElevTP3	1
angle3	deg min	sec		Backsi	ght		1
	Foresi	ht		BS1	n		
Station	Rod	In	erval	BS2	ft		
Sta2	Rod2	82	n	BS3	n		
Sta3	Rod3	S 3	ß	Sum BS	Check		
Sta4	Rod4	54	n	Foresi	ght		
The	Vertical angles			FS2	ft		
Vangle2	ana la suto la			FS3	n		
Vangle3	deg min	Nec		FS4	ft		
Vangle4	deg min	Nec		Sum FS	Check		
and a start of the	arg min i	Sec		Z = (SumBS - Su	nFS)		Check
Knowns				Q = Elev Final poin	t (TBM4) - Elev First Pois	t (TBM3)	Check
		Calcu	lation	N=(Z - Q)			Check
Lev IBM3	n						
				Ba	ck		Next
		4					

Figure (11/a): Leveling (4 Stations).

		Nur	nber 2		Volum	e 15 Ju	ine 2009		Jour	nal of En	gineering	
Levelin	ıg (4 Stations	;)										
nput							Output					
			Backsight				Vertical	Distances for Backs	sight	He	ight Instrument	
S	tation]	Rod		Interval		Vdl	2,28339192868951	fi	HII	1410.48339192869	fì
Stal	твмз	Rodl	8.6	S1	3.14	ft	Vd2	35 7722155099583	fi	HI2	1463 09667832923	fi
Sta2	TP1	Rod2	4.5	S2	6.32	ft	7/43	C 00000040001050	 	LIIB	1503 55000310345	
Sta3	TP2	Rod3	10	S 3	3.88	ft	Vertica	Distances for Fores	ight	Elev	ration of Stations	n
	The Vert	tical angle	es				Vd2	.15.0410708905804	ft	ElevTP1	1431 82446281927	fi
Vangle	l +0 de	g 25	min 00	sec			Vd3	-55.258213233242	ft	ElevTP2	1520.55489156247	fì

Vangle2	+3 deg	15	min 00	sec			Vd4	-1.91344439266989	ft	ElevTP3	1510.47224649512	fi
Vangle3	-1 deg	02	min 00	sec				Backsight			,	
			Foresigh	ıt			BS1	-6.31660807131049	fi			
Sta	ntion		Rod		Interval		BS2	31.2722155099583	ft			
Sta2	TP1	Rod2	6.3	S2	4.62	ft	BS3	-16.9960894600165	fi			
Sta3	TP2	Rod3	2.2	S 3	5.04	ft	Sum BS	7.9595179786313 Ch	eck			
Sta4	TBM4	Rod4	5	S4	5.06	ft		Foresight				
	The Vert	tical angl	les				FS2	-21.3410708905804	fì			
Vangle2	-1 de	g 52	min 00	sec			FS3	-57.458213233242	fì			
Vangle3	-6 de	g 20	min 00	sec			FS4	-6.91344439266989	fi			
Vangle4	-0 de	g 13	min 00	sec			Sum FS	-85.712728516492 Ch	eck			
Kı	nowns						Z = (Sum	BS - SumFS)		93.	6722464951238 Chec	k
ĸ	100						Q = Elev Fi	inal point (TBM4) - Elev	First Poin	(TBM3) 93.	6722464951235 Chec	k
ElevTBM3	1416.8	ft		Cal	culation		$\mathbf{N} = (\mathbf{Z} - \mathbf{Q})$)		0	Chec	k
	,							1			1	
								Back			Next	
			Save					Dist	in a Du	- f ile		
		_						Plou	ing Pr	оше		

Plotting Pro Figure (11/b): Leveling (4 Stations) Input and Computation [4].

When this option is selected the figure shown in figures (10/b) and (11/b) presented to the user. The user has to input the following information:

- Distances (D1, D2, and D3,....).
- Elevation of Stations (ElevTBM2, ElevTP1, and ElevTP2,.....).
- Scale (S).

When these data are input the computer program and when the user selects "**plotting profile**" button to begin by drawing the points are illustrated in the below figures (12/a),(12/b),(12/c),and figure (12/d). The program output result is saved for later use by the user in a text file.

	Distances	Eleva	tion of stations	S	cale
DI	[100	ElevTBM2	1416.800	Xmax	1000
D2	200	ElevTP1	1431.824	Ymax	2000
D3	300	ElevTP2	1520.555		,
	C			Plott	ing Profile Back



Conclusions:

From the results obtained in research, the following conclusions can be made:-

1. The stadia measurement is modeled by Visual Basic language as software named **MSM** (<u>M</u>odeling the <u>S</u>tadia <u>M</u>easurements). The program is formulated and written by using Visual Basic, Version 6.

2. The software that were developed in this research has been tested by performing the stadia measurements method and proved to be efficient.

3. The solution problems of traversing and leveling in manual method is more complex if compared to Figure (12/c): Plotting Leveling (5 Stations) Input and Plotting.

4. The developed program (**MSM**) needs less time as compared to the manual method in order to solve the problem.

Reference: Figure (12/d): Plotting Leveling (6 Stations) Input and Plotting.

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